

VISCOUS DISSIPATION EFFECTS ON UNSTEADY HYDROMAGNETIC GAS FLOW  
ALONG AN INCLINED PLANE WITH INDIRECT NATURAL CONVECTION  
IN THE PRESENCE OF THERMAL RADIATION

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ABSTRACT

*In this paper, the viscous dissipation effects on unsteady gravity-driven thermal convection flow of a viscous incompressible, electrically-conducting, absorbing-emitting, optically-thick gray gas along an inclined plane in the presence of thermal radiation has been carried out. The Rossel and diffusion flux model is employed to simulate thermal radiation effects. The governing equations for this investigation are solved numerically by using Ritz FEM. The effects of Prandtl number ( $P_r$ ), Boltzmann-Rosseland radiation parameter ( $K_1$ ), Hartmann number squared ( $M^2$ ), Eckert number ( $E_c$ ), Grashof number ( $G_r$ ) and plate inclination ( $\alpha$ ) on the dimensionless velocity ( $u$ ) and temperature ( $\theta$ ) distributions are studied. Results obtained show that a decrease in the velocity and temperature distributions as the Prandtl number increased. The velocity and temperature are enhanced as Boltzmann-Rosseland radiation parameter and Grashof number are increased.*

**Key words:** Eckert number, Boltzmann-Rosseland radiation parameter, free convection, thermal radiation, Ritz FEM.

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## 1. INTRODUCTION

Radiative convection flows are encountered in many areas of industrial and environmental processes. e.g., heating and cooling chambers, fossil fuel combustion energy processes, evaporation for large open water reservoirs, astrophysical flows, solar power technology and space vehicle re-entry. Also, many areas of technology and applied physics including oxide melt materials processing, astrophysical fluid dynamics, plasma flows switch performance, MHD energy pumps operating at very high temperatures and hypersonic aerodynamics. Bestman and Adjepong [1] studied the unsteady hydromagnetic free-convection flow with radiative heat transfer in a rotating fluid. Raptis and Masslas [2] studied unsteady magneto-hydrodynamic convection in a gray, absorbing but non-scattering fluid regime using the Rosseland radiation model. Chamkha [3] investigated unsteady convective heat and mass transfer past a semi-infinite permeable moving plate with heat absorption, where it was found that increase in the solutal Grashof number enhanced the concentration buoyancy effects leading to increase in the velocity. Ganesan and Loganadan [4] presented Radiation and mass transfer effects on flow of an incompressible viscous fluid past a moving cylinder. Azzam [5] studied thermal radiation flux influence on hydromagnetic mixed free-forced convective steady optically-thick laminar boundary layer flow by using Rosseland approximation. Abd-El-nay *et al.* [6] presented the radiation effects on MHD free convection flow over a vertical plate with variable surface temperature by finite difference solution. Muthucumaraswamy and Janakiraman [7] presented MHD and radiation effects on moving isothermal vertical plate with variable mass diffusion. Gbadayan and idowu [8] studied the magneto-hydrodynamic heat transfer between two concentric rotating spheres employing the optically thin limit case for thermal radiation. Heat and mass transfer of an unsteady MHD free convection flow of rotating fluid past a vertical porous flat plate in the presence of radiative heat transfer studied by Mbeledogu and Ogulu [9]. Muthucumaraswamy *et al.* [10] studied unsteady flow past an accelerated infinite vertical plate with variable temperature and uniform mass diffusion.

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Viscous mechanical dissipation effects are important in geophysical flows and also in certain industrial operations and are usually characterized by Eckert number. Gebhart [11] presented the importance of viscous dissipative heat in a free convection flow in the case of isothermal and constant heat flux at the plate. Gebhart and Molledorf [12] presented the effects of viscous dissipation for external natural convection flow over a surface. Viscous dissipation heat on the two dimensional unsteady free convective flow past an infinite vertical porous plate when the temperature oscillates in time and there is constant suction at the plate was studied by Soundalgekar [13]. Gokhale and Samman [14] presented the effects of mass transfer on the transient free convection flow of a dissipative fluid along a semi-infinite vertical plate with constant heat flux. Cookey *et al.* [15] studied the influence of viscous dissipation and radiation on an unsteady MHD free convection flow past an infinite heated vertical plate in a porous medium with time dependent suction. Zueco Jordan [16] presented the radiation and viscous dissipation effects on MHD unsteady free convection over vertical porous plate by network simulation method. Mohamoud [17] presented temperature dependent viscosity effects in transient dissipative radiation hydrodynamic convection, showing that an increase in Eckert number and decrease in air viscosity accelerate the flow, whereas increasing magnetic field or thermal radiation flux decelerates the flow. Hitesh Kumar [18] studied the boundary layer steady flow and heat transfer of a viscous incompressible fluid due to a stretching plate with viscous dissipation effect in the presence of transverse magnetic field. Recently, Mass transfer effects on an unsteady MHD free convective flow of an incompressible viscous dissipative fluid past an infinite vertical porous plate studied by Reddy [19]. Reddy and Sunzu [20] presented thermal radiation and viscous dissipation effects on MHD heat and mass diffusion flow past a surface embedded in a porous medium with chemical reaction.

The object of the present paper is to analyze the effects of viscous dissipation on unsteady gravity-driven thermal convection flow of a viscous incompressible, electrically-conducting, absorbing-emitting, optically-thick gray gas along an inclined plane in the presence of thermal radiation. The problem is governed by system of non-linear partial differential equations, whose exact solutions are difficult to obtain, whenever possible. Thus, the Ritz FEM is adopted for solution, which is more economical from a computational point of view. The behaviors of the velocity, temperature, frictional shearing stress and wall temperature gradient have been discussed for variations in the governing parameters.

## 2. MATHEMATICAL MODEL

Consider the transient hydro-magnetic flow of a viscous, incompressible, electrically conducting, absorbing-emitting, non-scattering, optically-thick gas along an infinite plate inclined at angle  $\alpha$  to the horizontal is considered. The plate moving with constant velocity  $u_0$ . Refractive index of the gas medium is constant. A uniform magnetic field  $B_0$ , applied normal to the plate. The  $x'$ -axis oriented along the plate and the  $y'$ -axis perpendicular to the plate. The Maxwell's field equations comprise five vector equations - the Ampere's law, magnetic field continuity, Faraday's law, Kirchhoff's law and Ohm's law. The generalized equations in vector form, for flow of an electrically-conducting gas are the Maxwell equations:

$$\nabla \times B = \mu J \quad \text{Ampere's law} \quad (1)$$

$$\nabla \cdot B = 0 \quad \text{Magnetic Field Continuity (Maxwell Equation)} \quad (2)$$

$$\nabla \times E = -\frac{\partial B}{\partial t} \quad \text{Faraday's law} \quad (3)$$

$$\nabla \cdot J = 0 \quad \text{Kirchhoff's law} \quad (4)$$

$$J = \sigma [E + v \times B] \quad \text{Ohm's law} \quad (5)$$

where  $J$  is the current density,  $B$  is the magnetic field vector,  $\sigma$  is the electrical conductivity,  $E$  is the electrical field density vector,  $\rho$  is the density,  $v$  is the velocity vector,  $\mu$  is viscosity and  $t$  is time.

From an order of magnitude analysis, it can be shown that for two-dimensional ( $xy$ ) magneto-hydrodynamic gas dynamic flows, the hydromagnetic retarding force (Lorentz body force) acts only parallel to the flow and has the form:

$$F_{\text{magnetic}} \approx -\sigma B_y^2 u \quad (6)$$

where  $B_y$  is the component of magnetic field in the  $y$ -direction.

We consider an aerodynamic viscous flow where the magnetic field is sufficiently weak to sustain a small magnetic Reynolds number such that induced magnetic field effects can be neglected. Joule electro-heating and Hall current/ionslip effects are also neglected. The temperature of the gas in the regime is  $T'$  and an induced pressure gradient generated by indirect natural convection acts along the  $x'$ -direction. All the fluid properties are constant; the plate temperature is prescribed  $T_w'$  and is of sufficiently high magnitude that thermal radiation effects are significant.

In accordance with the Boussinesq approximation, all fluid properties are constant with the exception of the density variation in the buoyancy term. Unidirectional radiation flux  $Q_r$  is considered and it is assumed that  $\frac{\partial Q_r}{\partial y'} \gg \frac{\partial Q_r}{\partial x'}$ .

Under these assumptions, the mass, momentum and energy conservation equations for the regime with regard to indirect natural convection may be presented as follows.

$$\frac{\partial u'}{\partial x'} + \frac{\partial v'}{\partial y'} = 0 \quad (7)$$

$$\frac{\partial u'}{\partial t'} + u' \frac{\partial u'}{\partial x'} + v' \frac{\partial u'}{\partial y'} = -\frac{1}{\rho} \frac{\partial p}{\partial x'} + \nu \frac{\partial^2 u'}{\partial y'^2} - \frac{\sigma B_0^2 u'}{\rho} + g \beta (T' - T_\infty) \sin a \quad (8)$$

$$0 = -\frac{1}{\rho} \frac{\partial p}{\partial x'} - g \beta (T' - T_\infty) \cos a \quad (9)$$

$$\frac{\partial T'}{\partial t'} = \frac{k}{\rho C_p} \frac{\partial^2 T'}{\partial y'^2} - \frac{1}{\rho C_p} \frac{\partial Q_r}{\partial y'} + \frac{\nu}{C_p} \left( \frac{\partial u'}{\partial y'} \right)^2 \quad (10)$$

Subject to the following initial and boundary conditions:

$$\begin{aligned} t' \leq 0: \quad u' = 0, T' = T_\infty \quad \text{for all } y' \geq 0 \\ t' > 0: \quad u' = u_0, T' = T_w \quad \text{for } y' = 0 \\ u' \rightarrow 0, T' \rightarrow T_\infty \quad \text{as } y' \rightarrow \infty \end{aligned} \quad (11)$$

where  $u'$  is the velocity in the  $x'$ - direction,  $v'$  is velocity in the  $y'$ - direction,  $g$  is acceleration due to gravity,  $\nu$  is the kinematic viscosity of the optically-dense gas,  $T'$  is temperature of the fluid,  $T_\infty$  is free stream temperature of the fluid,  $T_w$  is plate surface temperature,  $\rho$  is the density,  $C_p$  is specific heat at constant pressure,  $k$  is thermal conductivity of the optically-dense fluid,  $\beta$  is volumetric coefficient of thermal expansion,  $t'$  is time,  $B_0$  is uniform magnetic field,  $\sigma$  is electrical conductivity of the gas and  $Q_r$  is radiative heat flux.

In transient flow, the frictional (viscous) and gravitational forces do not balance exactly and the discrepancy is proportional to the acceleration of the fluid, the deviation between the free surface of the gas and the plate inclination also contributes to this and an instability mechanism arises in the inclined plane flow. There is pressure distribution in the flow with a gradient defined as:

$$\frac{\partial p}{\partial y'} = \rho g \quad (12)$$

From Eq. (3), integration gives:

$$p = \rho g \beta (h - y') (T' - T_\infty) \cos a \quad (13)$$

where  $h$  denotes free surface elevation. Differentiating Eq. (13) with respect to  $x'$  yields:

$$\frac{\partial p}{\partial x'} = \rho g \beta (T' - T_\infty) \frac{\partial h}{\partial x'} \cos a \quad (14)$$

Above the leading edge of the plate ( $x' = 0$ ), the density variation with depth is constant i.e., will remains unchanged

for all  $\frac{\partial h}{\partial x'}$ . we therefore prescribe the following condition:

$$\frac{\partial h}{\partial x'} = \text{cons} \tan t = F_1 \quad (15)$$

The following non-dimensional quantities introduced to transform equations (7) to (10) under the boundary conditions (11) into dimensionless form:

$$u = \frac{u'}{u_0}, y = \frac{u_0 y'}{\nu}, t = \frac{u_0^2 t'}{\nu}, \theta = \frac{T' - T_\infty}{T_w - T_\infty}, P_r = \frac{\mu C_p}{k}, M = \frac{\sigma B_0^2 \nu}{\rho u_0^2}, \mu = \rho \nu,$$

$$E_c = \frac{u_0^2}{C_p (T_w' - T_\infty')}, G_r = \frac{g \beta v (T_w' - T_\infty')}{u_0^3} \quad (16)$$

where  $u$  is dimensionless velocity in the  $x$ - direction,  $t$  is non-dimensional time,  $y$  is dimensionless transverse coordinate,  $\theta$  is dimensionless temperature,  $G_r$  is the Grashof number,  $P_r$  is the Prandtl number,  $E_c$  is the Eckert number and  $M$  denotes the square root of the Hartmann hydro-magnetic number.

Introducing the above non-dimensional variables into Eqs. (8) and (9) using Eq. (15) also, and neglecting convective acceleration terms, we get in due course at the dimensionless form of the momentum equation:

$$\frac{\partial u}{\partial t} = G_r (\sin a - F_1 \cos a) \theta + \frac{\partial^2 u}{\partial y^2} - M^2 u \quad (17)$$

The radiative heat flux vector is addressed using the Rosseland diffusion flux approximation is therefore used leading to a Fourier type gradient function viz:

$$Q_r = -\frac{4\sigma}{3k^*} \frac{\partial T'^4}{\partial y'} \quad (18)$$

where  $\sigma$  is the Stefan-Boltzmann constant and  $k^*$  is the spectral mean absorption coefficient of the medium. Considering the temperature differences within the flow sufficient small,  $T'^4$  can be expressed as the linear function of temperature  $T'$ . This is accomplished by expanding  $T'^4$  in a Taylor series about a free stream temperature  $T_\infty'$  and neglecting the higher-order terms,

$$T'^4 \cong 4T_\infty'^3 T' - 3T_\infty'^4 \quad (19)$$

By using equations (16) and (19), equation (10) reduces to

$$\frac{\partial \theta}{\partial t} = \left( \frac{1 + K_1}{P_r} \right) \frac{\partial^2 \theta}{\partial y^2} + E_c \left( \frac{\partial u}{\partial y} \right)^2 \quad (20)$$

where  $K_1 = \frac{16\sigma T_\infty'^3}{3k^*k}$  denotes the Boltzmann-Rosseland radiation conduction number.

This parameter  $K_1$  embodies the relative contribution of heat transfer by thermal radiation to thermal conduction; large  $K_1$  ( $>1$ ) corresponds to thermal radiation dominance and small  $K_1$  ( $<1$ ) to the thermal conduction dominance. For  $K_1 = 1$  both conduction and radiative heat transfer modes contributes equally to the regime. Clearly the second term in Eq.(20) is an augmented diffusion term i.e., with  $K_1 = 0$ , thermal radiation vanishes and Eq. (20) reduces to the familiar unsteady one-dimensional conduction-convection equation. The boundary conditions Eq.(11) are also transformed using (16) to:

$$\begin{aligned} t \leq 0: \quad u = 0, \theta = 0 & \quad \text{for } y \geq 0 \\ t > 0: \quad u = 1, \theta = 1 & \quad \text{for } y = 0 \\ u \rightarrow 0, \theta \rightarrow 0 & \quad \text{as } y \rightarrow \infty \end{aligned} \quad (21)$$

### 3. METHOD OF SOLUTION

Equations (17) and (20) are non-linear system of partial differential equations to be solved under the initial and boundary conditions of equation (21) However, whose exact or approximate solutions are not possible. Hence, the Ritz finite element method is applied to solve these equations. The method entails the following steps.

1. Division of the whole domain into smaller elements of finite dimensions called "finite elements".
2. Generation of the element equations using variational formulations.
3. Assembly of element equations as obtained in step 2.
4. Imposition of boundary conditions to the equations obtained in step 3.
5. Solution of the assembled algebraic equations.

The assembled equations can be solved by any of the numerical technique viz. Gauss-seidal iteration method. An important consideration is that of shape functions which are employed to approximate actual functions. For one dimensional and two dimensional problems, the shape functions can be linear/quadratic and higher order. However, the suitability of the shape functions varies from problem to problem. Due to simple and efficient use in computations linear shape functions are used in the present problem. Here, the boundary condition  $y \rightarrow \infty$  is approximated by  $y = 10$ , which is sufficiently large for the velocity to approach convergence criterion. To prove convergence and stability of the Ritz FEM, the computations are carried out by making small changes in time  $t$  and  $y$  – directions. For these slightly changed values, no significant change was observed in the values of velocity ( $u$ ) and temperature ( $\theta$ ). Hence, the Ritz FEM is convergent and stable.

The frictional shearing stress at the plate surface ( $y = 0$ ) and the wall temperature gradient are defined as:

$$\left( \frac{du}{dy} \right)_{y=0} \text{ and } \left( \frac{d\theta}{dy} \right)_{y=0}$$

#### 4. NUMERICAL RESULTS AND DISCUSSION

The problem of unsteady gravity-driven thermal convection flow of a viscous incompressible, electrically-conducting, absorbing-emitting, optically-thick gray gas along an inclined plane in the presence of thermal radiation taking into account viscous dissipation is addressed in this study. The numerical calculation has been carried out for dimensionless velocity ( $u$ ), dimensionless temperature ( $\theta$ ), frictional shearing stress and temperature gradient for various values of the material parameters. Numerical results are presented in figures and tables. These results show the effect of the material parameters on the quantities mentioned.

Figure 1 and 2 shows the effects of Prandtl number  $P_r$  on the temperature distribution and velocity with transverse coordinate ( $y$ ) for  $P_r = 0.71$ , which corresponds to air,  $P_r = 1.00$ , which corresponds to electrolytic solution and  $P_r = 7.00$ , which corresponds to water, respectively. It is observed that an increase in the Prandtl number leads to decrease in both temperature and velocity. This is due to the fact that thermal conductivity of the fluid decreases with increasing Prandtl number results a decrease in the thermal boundary layer thickness. The effects of Boltzmann-Rosseland radiation convection parameter ( $K_1$ ) on the temperature distribution and velocity are presented in Fig. 3 and 4, respectively. It is seen that an increasing values of  $K_1$  leads to increase in the temperature and velocity. For  $P_r = 0.71$  i.e.,  $P_r < 1$ , heat diffuses faster than momentum in the regime.  $K_1$  corresponds to an increase in the relative contribution of thermal radiation heat transfer to thermal conduction heat transfer. As for  $K_1 \ll 1$ , thermal conduction heat transfer will dominate and vice versa for  $K_1 > 1$ . Larger values of  $K_1$  therefore physically correspond to stronger thermal radiation flux and in accordance with this, the maximum temperature is observed for  $K_1 = 3$ . Also, temperature profiles all decay monotonically from the maximum at the plate to the free stream. Fig. 5 and 6 shows the effects of viscous dissipation parameter i.e., Eckert number  $E_c$  on the temperature distribution and velocity respectively, with  $K_1 = 1.0$  (i.e., radiation and conduction contributions are equal). It is observed that an increase in the Eckert number leads to increase in the temperature and velocity profiles. This is due to the effect of viscous dissipation on flow field is to increase the energy, yielding a greater fluid temperature and as a consequence greater buoyancy force. The effects of Hartmann number square root ( $M$ ) on the velocity distribution with distance normal to the plate ( $y$ ) are presented in Fig. 7. The hydromagnetic term in Eq. (17), i.e.,  $-M^2 u$  is a linear drag force term. With increasing magnetic field strength  $B_0$ ,  $M$  is increased and this serves to decelerate the flow along the inclined plate. Also, observed that the velocity profiles are strongly reduced with increasing values of  $M$ . Further, we note that as  $M$  rises, the velocity profiles decreases to zero progressively for shorter distance from the plate surface. Fig. 8 depicts the effects of free convection parameter i.e., Grashof number  $G_r$  on the velocity distribution with distance normal to the plate ( $y$ ). It can be seen that an increase in the Grashof number leads to increase in the velocity. Free convection currents as simulated with the buoyancy term serve to accelerate the flow along the inclined plate. The effects of plate inclination ( $\alpha$ ) on the velocity distribution with distance normal to the plate ( $y$ ) are presented in Fig.9. It can be seen that an increase in the plate inclination values increases the velocity profiles. A gradual decrease occurs

from the plate to the free stream. Velocity becomes negative further from the plate surface for lower angle of inclination i.e., back flow arises. Also, we observe that an increase in angle of inclination to  $45^\circ, 60^\circ$  and to the maximum (vertical) orientation of  $a = 90^\circ$ , the flow is strongly accelerated.

Table 1 shows the effects of Prandtl number ( $P_r$ ), Boltzmann-Rosseland radiation-convection parameter ( $K_1$ ), and viscous dissipation parameter i.e., Eckert number ( $E_c$ ) on the frictional shearing stress and plate temperature gradient, respectively. It is observed that an increase in the Prandtl number leads to decrease in the frictional shearing stress and increase in the wall temperature gradient. As increase in the Boltzmann-Rosseland radiation parameter and Eckert number increases in the frictional shearing stress and decrease in the wall temperature gradient. The effects of Hartmann number square root ( $M$ ), free convection parameter i.e., Grashof number ( $G_r$ ), and plate inclination ( $a$ ) on the frictional shearing stress are presented in table 2. It can be seen that an increase in the square root of Hartmann number ( $M$ ) leads to decrease in the frictional shearing stress whereas an increase in the Grashof number and plate inclination increases the frictional shearing stress. Here, increasing plate inclination serves to accelerate the flow and shearing stress magnitude strongly increased with rise in the Grashof number. Negative values indicate that back flow.

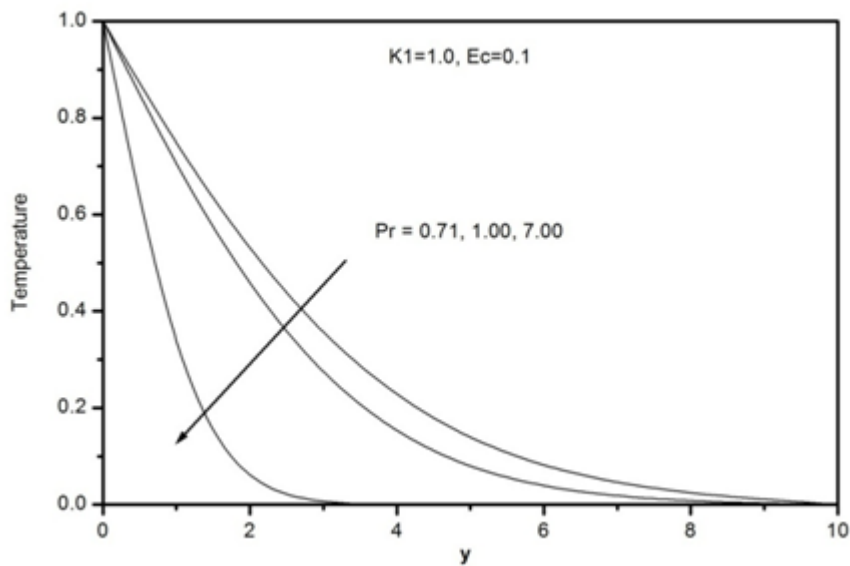


Figure-1: Effects of Prandtl number  $P_r$  on the temperature ( $\theta$ )

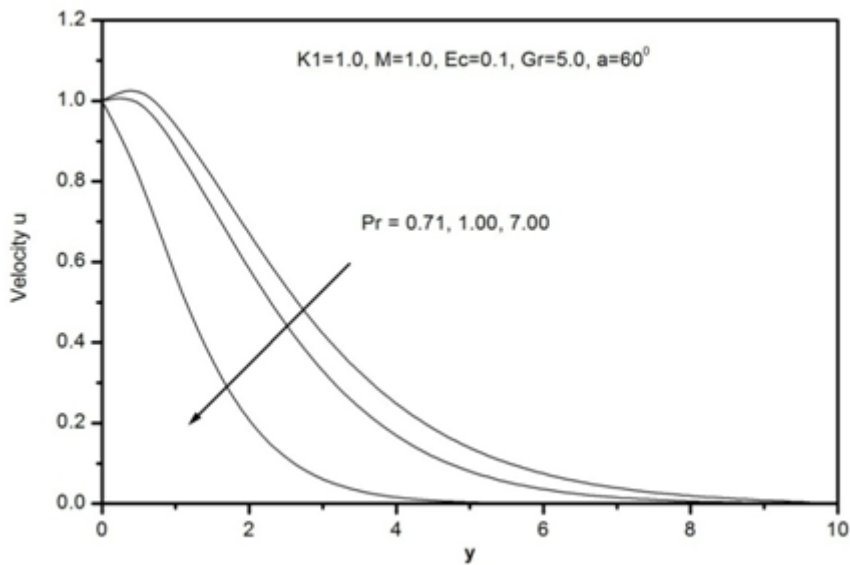


Figure-2: Effects of Prandtl number  $P_r$  on the velocity ( $u$ )

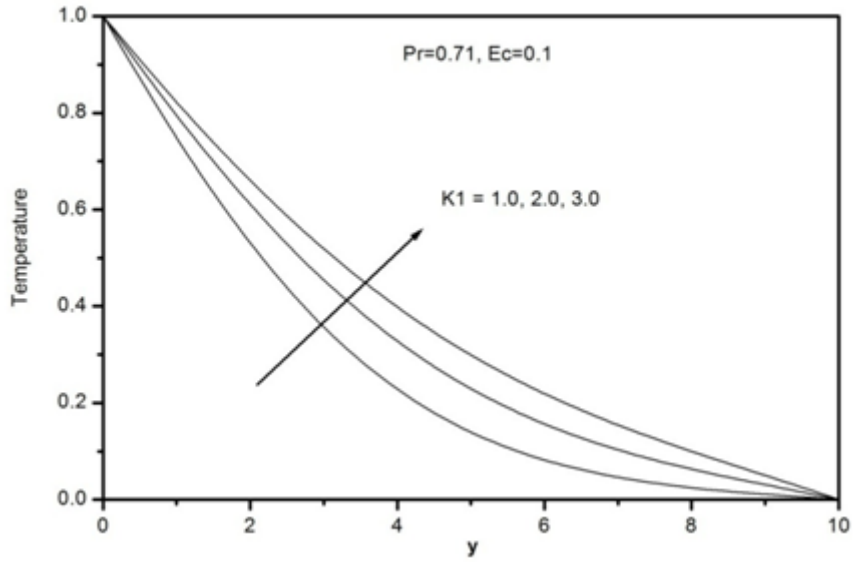


Figure-3: Effects of Boltzmann-Rosseland radiation parameter  $K_1$  on the temperature ( $\theta$ )

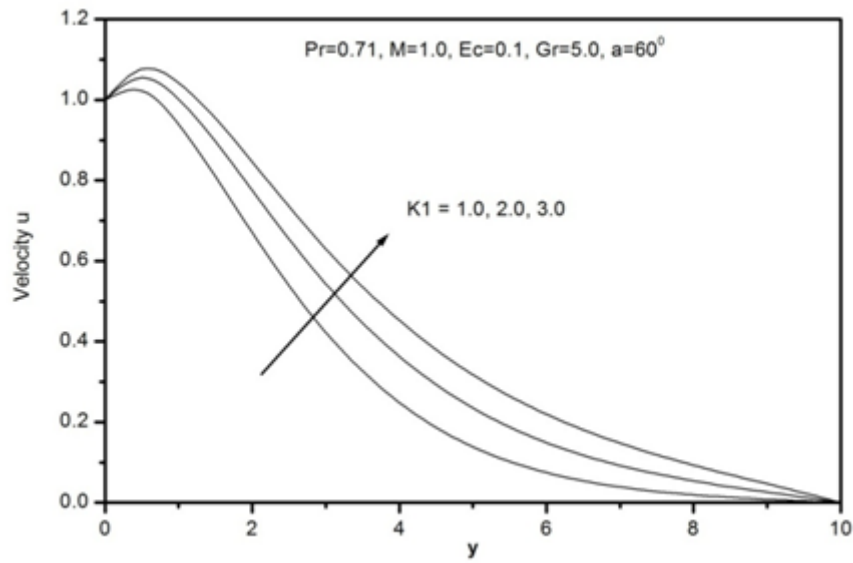


Figure-4: Effects of Boltzmann-Rosseland radiation parameter  $K_1$  on the velocity ( $u$ )

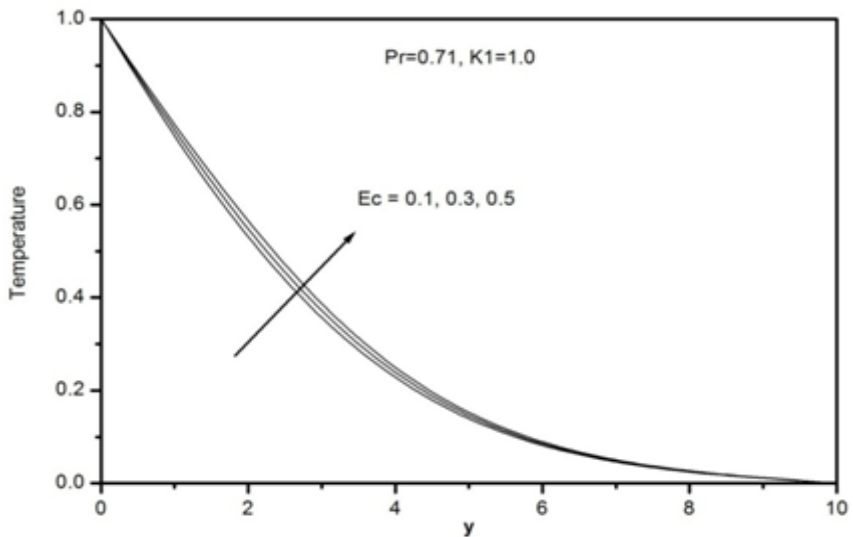


Figure-5: Effects of Eckert number  $E_c$  on the temperature ( $\theta$ )

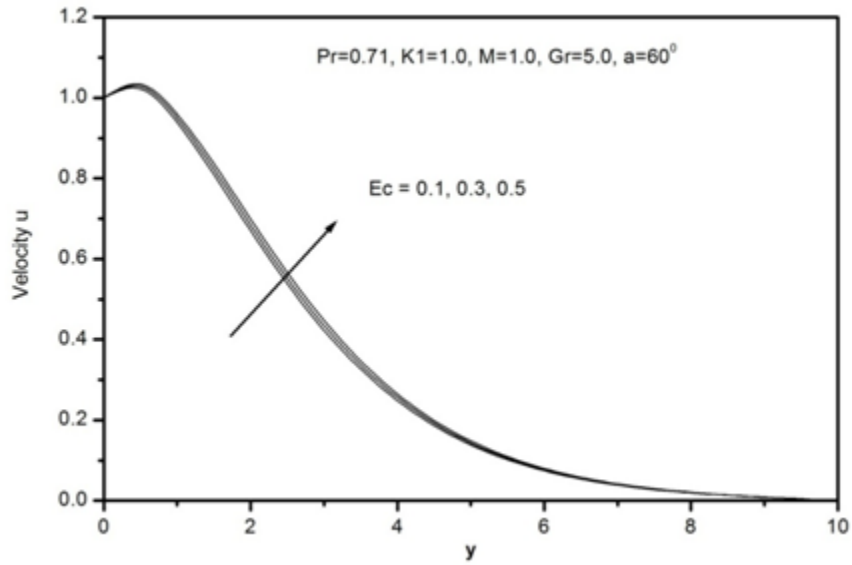


Figure-6: Effects of Eckert number  $E_c$  on the velocity ( $u$ )

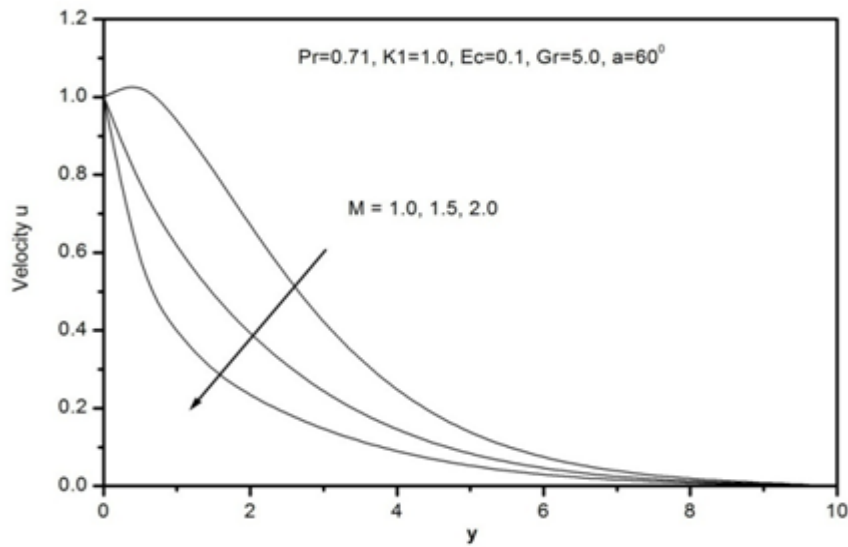


Figure-7: Effects of Hartmann number square root ( $M$ ) on the velocity ( $u$ )

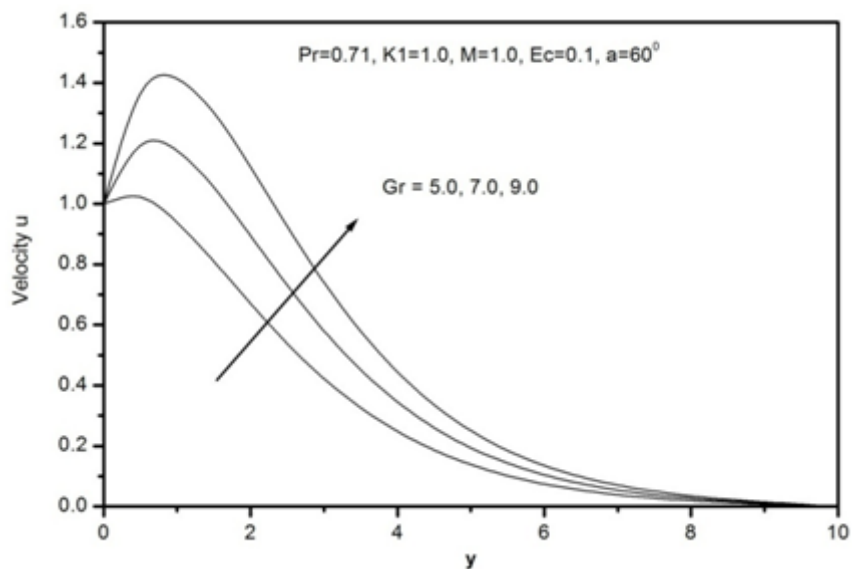
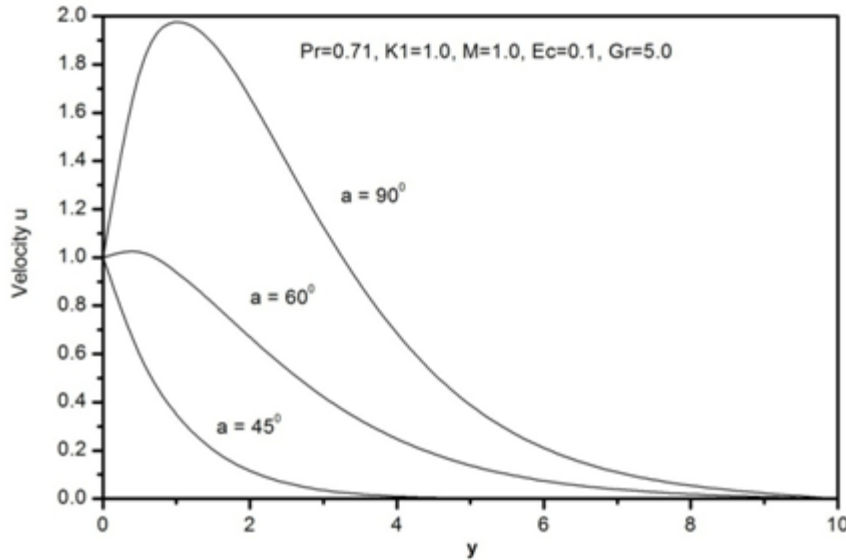


Figure-8: Effects of Grashof number  $G_r$  on the velocity ( $u$ )





**Figure-9:** Effects of plate inclination ( $a$ ) on the velocity ( $u$ )

**Table-1:** The numerical values of frictional shearing stress  $\left(\frac{du}{dy}\right)_{y=0}$  and wall temperature gradient  $\left(\frac{d\theta}{dy}\right)_{y=0}$  for various values of  $P_r, K_1$  and Eckert number  $E_c$ .

$P_r$	$K_1$	$E_c$	$\left(\frac{du}{dy}\right)_{y=0}$	$\left(\frac{d\theta}{dy}\right)_{y=0}$
0.71	1.0	0.1	0.044770	0.257590
1.00	1.0	0.1	-0.013256	0.303190
0.71	2.0	0.1	0.110220	0.209792
0.71	1.0	0.3	0.056288	0.244470

**Table-2:** The numerical values of frictional shearing stress  $\left(\frac{du}{dy}\right)_{y=0}$  for various values of  $M, G_r$  and plate inclination ( $a$ ).

$M$	$G_r$	$a$ (degrees)	$\left(\frac{du}{dy}\right)_{y=0}$
1.0	5.0	60	0.044770
2.0	5.0	60	-0.833416
1.0	7.0	60	0.387422
1.0	5.0	90	1.541034

## 5. CONCLUSIONS

In this paper, the governing equations has been examined for unsteady gravity-driven thermal convection flow of a viscous incompressible, electrically-conducting, absorbing-emitting, optically-thick gray gas along an inclined plane taking into account viscous dissipation in the presence of thermal radiation and a transverse magnetic field effects. The Rosseland diffusion flux model is employed to simulate thermal radiation effects. Employing the Ritz FEM, the leading equations have been solved numerically. We can conclude from these results that an increase in the Prandtl number and the Hartmann number square root leads to decrease in the velocity and temperature. An increase in the Eckert number increases in both velocity and temperature distributions. The velocity and temperature increased as Boltzmann-Rosseland radiation parameter and Grashof number are increased. Also, an increase in the plate inclination values increases the velocity and the maximum (vertical) orientation of  $a = 90^\circ$ , the flow is strongly accelerated (Fig.9).

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