## **COMPUTATIONAL TREATMENTS OF AN IMPROVED** CONJUGATE GRADIENT METHOD FOR UNCONSTRAINED MINIMIZATION

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## ABSTRACT

**R**ecently, the authors introduced a new three-terms nonlinear Conjugate Gradient (CG) method [2] for solving unconstrained optimization problems. Their method was compared with the well-known Zhang's three-terms CGmethod [32]. This paper contains a description of several new restarting procedures for the same proposed CG-method introduced by the authors and a numerical investigation of the influence of several scaling techniques with a modified perfect cubic line search procedure on their efficiency. Computational results obtained by means of (35) sufficiently difficult problems are given with promising numerical results.

Key Words: Conjugate Gradient Method, Unconstrained Optimization, Convergence Property, Line Searches, Restarting and Scaling Techniques, Large-Scale Problems, Computational Numerical Experiments.

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#### 1. INTRODUCTION:

In this study, we are concerned with the minimization of an unconstrained optimization problem to find a local minimum  $x^* \in \mathbb{R}^n$  of the function  $f: X \to \mathbb{R}$  on an open set  $X \subset \mathbb{R}^n$ ; i.e. a point  $x^* \in \mathbb{R}^n$  that satisfies the inequality  $f(x^*) \le f(x) \quad \forall x \in B(x^*, \varepsilon)$  for some  $\varepsilon > 0$ , where  $B(x^*, \varepsilon) = \left\{x \in \mathbb{R}^n : \|x - x^*\| < \varepsilon\right\} \subset X$  is an open ball contained in  $X \subset \mathbb{R}^n$ : in other words we want to:

$$\min\left\{f(x)\middle| x \in \mathbb{R}^n\right\} \tag{1}$$

where  $f: \mathbb{R}^n \to \mathbb{R}$  is a continuously differentiable function, and its gradient at point  $x_k$  is denoted by  $g_k$  for the sake of simplicity. n is the number of variables, which is automatically assumed to be large. The iterative formula of nonlinear CG-method is given by:

$$x_k = x_{k-1} + \alpha_k d_k, \tag{2}$$

where  $\alpha_k$  is a step-length, and  $d_k$  is a search direction which is determined by:

$$d_{k} = \begin{cases} -g_{0}, & \text{if } k = 0, \\ -g_{k} + \beta_{k} d_{k-1}, & \text{if } k \ge 1, \end{cases}$$
(3)

where  $\beta_k$  is a scalar and  $d_k$  is a direction vector satisfying the equation  $Bd_k + g_k = 0$ , where B is a symmetric positive definite approximation of the Hessian matrix that is constructed iteratively [18]. If the number of variables is large, then matrix B cannot be stored, nor factored in a reasonable time, so other methods have to be used. There exist several classes of such methods: Conjugate Gradient (CG) methods [9], difference versions of Truncated Newton (TN) methods [8], Variable Metric (VM) methods with limited storage [20], sparse variants of VM-methods [27], and partitioned VM-methods for separable problems [12]. The last two classes require the special structure of optimization

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problems. From the other classes the simplest are the CG-methods which need only 3-5 n-dimensional vectors (it depends on their implementation). Recently new attention has been given to these methods because they are globally convergent with mild and reasonable assumptions. Their idea starts since 1952, there have been many well-known formulas for the scalar  $\beta_k$ , for example, Fletcher-Reeves (FR), Polak-Ribiere (PR), Hestenes-Stiefel (HS) and Dai-Yuan (DY) [6, 21]:

$$\beta_{k}^{FR} = \frac{\left\|g_{k}\right\|^{2}}{\left\|g_{k-1}\right\|^{2}}, \quad \beta_{k}^{PR} = \frac{g_{k}^{T} y_{k-1}}{\left\|g_{k-1}\right\|^{2}}, \quad \beta_{k}^{HS} = \frac{g_{k}^{T} y_{k-1}}{d_{k-1}^{T} y_{k-1}}, \quad \beta_{k}^{DY} = \frac{\left\|g_{k}\right\|^{2}}{d_{k-1}^{T} y_{k-1}}, \quad (4)$$

where  $y_{k-1} = g_k - g_{k-1}$ , symbol  $\| \cdot \|$  denotes the Euclidean norm of vectors. If f is a strictly convex quadratic function, all these methods are equivalent in the case that an Exact Line Search (ELS) is used. If the objective function is non-convex, their behaviors may be distinctly different. In the past two decades, the convergence properties CG-methods defined in (4) have been intensively studied by many researchers [1, 5, 11, 13, 14, 16, 26, 29, 33]. Although the HS method is most general and the FR method is the simplest with good global convergence properties (theoretical), the most numerically efficient was proved to be the PR method. Another important issue related to the performance of CG-methods is the line search, which requires sufficient accuracy to ensure that the search directions yield descent [15]. Common criteria for line search accuracy are the Wolfe conditions [30, 31]:

$$f(x_{k-1} + \alpha_k d_k) - f(x_{k-1}) \le -\delta \alpha_k g_{k-1}^T d_{k-1},$$
(5a)

$$g_k^T d_{k-1} \ge \sigma g_{k-1}^T d_{k-1}, \tag{5b}$$

where  $0 < \delta \le \sigma < 1$ . In the "Strong Wolfe" conditions, (5b) is replaced by

$$\left|g_{k}^{T}d_{k-1}\right| \leq -\sigma g_{k-1}^{T}d_{k-1} \,. \tag{5c}$$

It has been shown [7] that for the FR scheme, the strong Wolfe conditions may not yield a direction of descent unless  $\sigma \le 1/2$ . However, The CG-methods are more sensitive to their implementation than the VM methods:

- 1. The initial estimate  $\alpha_1$  of  $\alpha_k$  in the line search algorithm does not have theoretical justification for CG-methods. Therefore the CG-methods are more sensitive to the initial estimate  $\alpha_1$  than the VM methods.
- 2. CG-methods need more perfect line search than VM methods. We usually use  $\delta = 0.1$  for CG- VM-methods.
- 3. CG-methods strongly depend on restarts while VM-methods need not be restarted.

## 2. PRELIMINARIES:

2.1. Assumption: The objective function f is bounded below, and the level set

$$F = \left\{ x \in \mathbb{R}^n \left| f(x) \le f(x_0) \right\} \text{ is bounded.}$$
(6)

**2.2.** Assumption: In some neighborhood N of F, f is differentiable and its gradient is Lipschitz continuous, namely, there exists a positive constant L such that:

$$\left\|g(x) - g(y)\right\| \le L \left\|x - y\right\|, \quad \forall x, y \in N$$
(7a)

The above assumption implies that there exists a positive constant  $\overline{\gamma}$  such that

$$\left\|g(x)\right\| \le \overline{\gamma}, \quad \forall x \in F \tag{7b}$$

## 2.3. Zhang's Three-Terms CG-Method [32]:

Zhang, et al. had introduced a three-term CG method as follows:

$$d_{k} = \begin{cases} -g_{0}, & \text{if } k = 0, \\ -g_{k} + \beta_{k}^{DL} d_{k-1} - \xi_{k} \left( y_{k-1} - ts_{k-1} \right), & \text{if } k \ge 1, \end{cases}$$
(8a)

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where

$$t \ge 0; \qquad \xi_k = \frac{g_k^T d_{k-1}}{d_{k-1}^T y_{k-1}} \text{ and } \beta_k^{DL} = \frac{g_k^T (y_{k-1} - ts_{k-1})}{d_{k-1}^T y_{k-1}}, \tag{8b}$$

They show that the sufficient descent condition also holds true if no line search is used, that is,

$$g_{k-1}^{T}d_{k} = -\|g_{k-1}\|^{2}.$$
(9)

In order to achieve the global convergence result, Grippo and Lucidi [13] proposed a new line search. For given constants  $\tau > 0$ ,  $\delta > 0$ , and  $\lambda \in (0,1)$ , let

$$\alpha_k = \max\left\{\lambda^{j} \left(\frac{\tau \left|g_k^T d_k\right|}{\left\|d_k\right\|^2}\right); \quad j = 0, 1, \ldots\right\}$$
(10a)

satisfy

$$f(x_k) \le f(x_{k-1}) - \delta \alpha_k^2 \left\| d_{k-1} \right\|^2$$
 (10b)

This line search will be preferred to the classical Armijo one for the sake of a greater reduction of objective function. Introducing this line search rule, we are now ready to state the outline of the Zhang, et al. [32] first three-term CG-method as follows:

## 2.4. Outline of Zhang's Three-Terms CG-Algorithm [32]:

**Step 1.** Given  $x_0 \in \mathbb{R}^n$ . Let  $0 < \delta < \sigma < 1$ ,  $t \ge 0$  and  $d_0 = -g_0$ . Set k := 0.

**Step 2.** If  $||g_k|| \le 10^{-6}$ , then stop.

**Step 3.** Compute  $d_k$  using (8).

**Step 4.** Find the step-length  $\alpha_k$  satisfying (11) and (12).

$$f(x_{k-1} + \alpha_k d_k) - f(x_{k-1}) \le -\delta \alpha_k^2 \|d_{k-1}\|^2,$$
(11)

$$g(x_{k-1} + \alpha_k d_k)^T d_k \ge \sigma g_{k-1}^T d_{k-1}.$$
(12a)

$$\left|g_{k}^{T}d_{k-1}\right| \leq -\sigma g_{k-1}^{T}d_{k-1} \tag{12b}$$

and set  $x_k = x_{k-1} + \alpha_k d_k$ .

**Step 5.** Set k := k + 1, go to Step 2.

#### 2.5. Al-Bayati and Altae Three-Term CG-Method [2]:

The search directions of this method are defined by; see Al-Bayati and Altae:

$$d_{k} = \begin{cases} -g_{0}, & \text{if } k = 0, \\ -g_{k} + \beta_{k}^{N} d_{k-1} - \xi_{k} \left( y_{k-1} - (2 \frac{\|y_{k-1}\|^{2}}{s_{k-1}^{T} y_{k-1}}) s_{k-1} \right), & \text{if } k \ge 1, \end{cases}$$
(13a)

where

$$\beta_k^N = \max\left\{\frac{g_k^T y_{k-1}}{d_{k-1}^T y_{k-1}}, 0\right\} - t_k \frac{g_k^T s_{k-1}}{d_{k-1}^T y_{k-1}},\tag{13b}$$

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and

$$\xi_{k} = \frac{g_{k}^{T} d_{k-1}}{d_{k-1}^{T} y_{k-1}}; \qquad t_{k} = 2 \frac{\|y_{k-1}\|^{2}}{s_{k-1}^{T} y_{k-1}} \ge 0$$
(13c)

It is easy to see that the sufficient descent condition (9) also holds true if no line search is used.

#### 2.6. Outline of Al-Bayati and Altae Three-Term CG-Algorithm [2]:

**Step 1.** Given  $x_0 \in \mathbb{R}^n$ . Let  $0 < \delta < \sigma < 1$ ,  $t \ge 0$  and  $d_0 = -g_0$ . Set  $k \coloneqq 0$ .

**Step 2.** If  $||g_k|| \le 10^{-6}$ , then stop.

**Step 3.** Compute  $d_k$  using (13).

**Step 4.** Find the step-length  $\alpha_k$  satisfying (11) and (12) and set  $x_k = x_{k-1} + \alpha_k d_k$ .

**Step 5.** Set k := k + 1, go to Step 2.

# 3. MODIFIED RESTARTING; SCALING AND LINE SEARCH TECHNIQUES IMPLEMENTED IN THE NEW PROPOSED CG-ALGORITHM:

In this section we are going to introduce several new restarting and several scaling techniques to improve the performance behavior of Al-Bayati and Altae [2] three-terms CG-algorithm and as follows:

#### 3.1. Different Restarting Techniques:

We limit our attention to the PR method, but the same considerations can be used for the HS method. Usually the PR method is implemented with periodic restarts. In [23], Powell points out that the PR method works better if it is restarted whenever

$$\beta_k^{PR} < 0. \tag{14}$$

The PR method with periodic restarts can be disadvantageous for some problems that require more restarts at the beginning of the iterative process. Also, convergence results noted in this paper that our computational experiments show that the PR method is more efficient if it is restarted not only when (14) holds, but also whenever:

$$\beta_k^{PR} \le \eta \beta_k^{FR} \tag{15}$$

and

$$\lambda \left\| \boldsymbol{g}_{k} \right\|^{2} \leq \boldsymbol{\omega} \tag{16}$$

where  $1 < \eta < 1/(2\sigma)$  is a suitable constant (we recommend  $\lambda = 10^{-8}$ ,  $\eta = 1.34$ ,  $\omega = 10^{-4}$  all recommended values given in this paper were obtained experimentally by means of extensive computations).

## 3.2. Different Scaling Techniques:

Another useful tool for improving CG methods is scaling, which was originally developed for VM methods [24]. The scaling consists in replacing (3) by:

$$d_{k} = \gamma_{k} \left( -g_{k} + \beta_{k} d_{k-1} - t_{k} s_{k-1} \right), \tag{17}$$

where  $\gamma_k$  is the scaling factor. This type of CG-methods are called spectral CG-methods. Then it found that the best value of this parameter:

$$\gamma_k = \frac{y_{k-1}^T s_{k-1}}{y_{k-1}^T y_{k-1}},\tag{18}$$

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Note that when we use (17) then PR; FR and DY have to be replaced by:

$$\beta_{PR} = \frac{1}{\gamma_k} \left( \frac{y_{k-1}^T g_k}{g_{k-1}^T g_{k-1}} \right), \tag{19a}$$

and

$$\beta_{FR} = \frac{1}{\gamma_k} \left( \frac{g_k^T g_k}{g_{k-1}^T g_{k-1}} \right),$$
(19b)

$$\beta_{DY} = \frac{1}{\gamma_k} \left( \frac{g_k^T g_k}{d_{k-1}^T y_{k-1}} \right)$$
(19c)

For the simplification of subsequent considerations, we have used the following scaling criterion to scale our new proposed three-terms CG-algorithm.

$$\gamma_k = \bar{\gamma}_1, \text{ if } \frac{y_{k-1}^T s_{k-1}}{y_{k-1}^T y_{k-1}} < \bar{\gamma}_1$$
 (20a)

$$\gamma_k = \bar{\gamma}_2, \quad \text{if} \quad \frac{y_{k-1}^T s_{k-1}}{y_{k-1}^T y_{k-1}} < \bar{\gamma}_2$$
(20b)

$$\gamma_k = \frac{y_{k-1}^T s_{k-1}}{y_{k-1}^T y_{k-1}}$$
, otherwise, (20c)

where  $0 < \bar{\gamma}_1 < 1 < \bar{\gamma}_2$  (we recommend  $\bar{\gamma}_1 = 0.005$  and  $\bar{\gamma}_2 = 200$ ). The bounds  $\bar{\gamma}_1$  and  $\bar{\gamma}_2$  serve for improvement of stability.

#### 3.3. Perfect Cubic Line Search Technique:

Since the CG-methods require more **perfect line search** than other methods, they are very sensitive to its realization. We have essentially used the standard cubic line search implementation; namely (a perfect cubic interpolation), which can be represented by the following algorithm:

**3.4. Line Search Algorithm:** Input data:  $\Delta > 0$ ;  $0 < \varphi_1 < \varphi_2 < 1$  and  $0 < \delta < \sigma < 1/2$ .  $\delta = 0.0001$ ;  $\sigma = 0.1$ ,  $\varphi_1 = 0.01$ ,  $\varphi_2 = 0.9$  and  $\Delta = 1000$ 

Step (1): Determine the initial estimate  $\alpha_1$  of  $\alpha_k$ . This is may be taken as:  $\alpha_1 = (1, or \min\left(1, 2\frac{f_{\min} - f_1}{s_1^T g_1}\right))$ and set  $(\psi_1 = 0, i = 1)$ 

**Step** (2): Set  $\alpha_i = \min(\alpha_i, \Delta/||s_k||)$ . Set  $\rho_i = \psi_i$  and  $\psi_i = \alpha_i$ . If the conditions (5a) and (5c) are satisfied with  $f_{k+1}$  and  $g_{k+1}$  replaced by  $f(x_k + \alpha_i s_k)$  and  $g(x_k + \alpha_i s_k)$  respectively, then set  $\alpha_k = \alpha_i$  and **terminate the computation**. If both (5a) and  $s_k^T g(x_k + \alpha_i s_k) < 0$ , hold then go to Step(3), else go to Step(4).

Step (3): If  $\alpha_i = \Delta / \| s_k \|$  then set  $\alpha_k = \alpha_i$  and terminate the computation, else determine the new estimate  $\alpha_i$  by cubic extrapolation. Set  $\alpha_i = \max(\alpha_i, \psi_i / \varphi_2)$ , set  $\alpha_i = \max(\alpha_i, \psi_i / \varphi_1)$ , and go to Step(2).

Step (4): Determine the new estimate  $\alpha_i$  by cubic interpolation. Set  $\alpha_i = \max(\alpha_i, \rho_i + \varphi_1(\psi_i - \rho_i))$ , set  $\alpha_i = \max(\alpha_i, \rho_i + \varphi_2(\psi_i - \rho_i))$ . **Step (5)**: If the conditions (5a) and (5c)) are satisfied, with  $f_{k+1}$  and  $g_{k+1}$  replaced by  $f(x_k + \alpha_i s_k)$  and  $g(x_k + \alpha_i s_k)$  respectively, then set  $\alpha_k = \alpha_i$  and terminate the computation. If both (5a) nd  $s_k^T g(x_k + \alpha_i s_k) < 0$ , hold then set  $\rho_i = \alpha_i$ , else set  $\psi_i = \alpha_i$ ; go to **Step(4)**.

## 3.5. Outline of the New Scaled Three-Term CG-Algorithm:

**Step 1.** Given  $x_0 \in \mathbb{R}^n$ . Let  $0 < \delta < \sigma < 1$ ,  $t \ge 0$  and  $d_0 = -g_0$ . Set k := 0.

**Step 2.** If  $||g_k|| \le 10^{-6}$ , then stop.

**Step 3.** Compute  $d_k$  using:

$$d_{k} = \gamma_{k} \begin{cases} -g_{0}, & \text{if } k = 0, \\ -g_{k} + \beta_{k} d_{k-1} - \left(\frac{g_{k}^{T} d_{k-1}}{d_{k-1}^{T} y_{k-1}}\right) \left(y_{k-1} - \left(2\frac{\|y_{k-1}\|^{2}}{s_{k-1}^{T} y_{k-1}}\right)s_{k-1}\right), & \text{if } k \ge 1, \end{cases}$$

$$(21)$$

 $\gamma_k$  is defined by (20) and  $\beta_k$  is defined in (13b)

**Step 4.** Find the step-length  $\alpha_k$  satisfying cubic line search Algorithm (3.4) and conditions (11) - (12) and set  $x_k = x_{k-1} + \alpha_k d_k$ .

**Step 5.** Do a restart step. If  $(\beta_k^{PR} < 0 \text{ or } \beta_k^{PR} \le \eta \beta_k^{FR} \text{ or } \lambda \|g_k\|^2 \le \omega$  ) then set

k := k + 1, and go to **Step 2**.

## 4. CONVERGENCE RESULTS:

It is well known that any CG-method with perfect line search (with (5c) where  $\sigma = 0$ ) finds the minimum of a quadratic function after at most n steps. This property implies that any convergent CG-method with asymptotically perfect line search and with periodic restart is n-step quadratically convergent [3]. This result is very useful because asymptotically perfect line search can be easily realized by both quadratic and cubic interpolations. The global convergence of CG methods can be assured by suitable restart rules. The simplest such rule is the so-called angle test which consists in setting  $\beta_k = 0$  in (3) whenever:

$$\cos\left(\frac{d_k^T g_k}{\|d_k\|\|g_k\|}\right) < \delta_0 \tag{22}$$

where  $\delta_0$  is a prescribed constant (usually  $\delta_0 = 10^{-3}$ ). A more complicated angle test is proposed in [25]. If the line search is asymptotically perfect, the global convergence of CG-methods can be assured by periodic restarts. The first global convergence result which does not depend on restarts has been obtained by Zoutendijk [34] and Powell [22], who proved that the FR method with perfect line search is globally convergent in the sense that

$$\liminf \|g_k\| = 0 \tag{23}$$

where  $\liminf \|g_k\|$  is taken over the iterative process (1). Later, Al-Baali [1] generalized this result to include the FR

method without perfect line search. He has shown that (22) holds for the FR method whenever  $\sigma < 1/2$  in (5). Recently great effort was devoted to generalizing this result to other CG methods. Touati-Ahmed and Storey [28] have shown that the iterative process (2) and (3) with a line search satisfying (5) is globally convergent if:

$$0 \le \beta_k^{PR} \le \eta \beta_k^{FR} \tag{24a}$$

For  $1 < \eta < 1/(2\sigma)$ . In this case, we have proposed also the following criterion to ensure the global convergence property, namely:

$$\lambda \left\| \boldsymbol{g}_{k} \right\|^{2} \leq \boldsymbol{\omega} \tag{24b}$$

hold in every iteration, where  $0 < \lambda$  and  $\omega > 0$  are suitable constants.

The proof given in [28] guarantee that, for  $\sigma \eta < 1$ , the following inequality:

$$g_{k-1}^{T}d_{k-1} \leq -\frac{1}{1-\sigma\eta} \|g_{k-1}\|^{2}$$
<sup>(25)</sup>

is satisfied at every iteration. Therefore the CG-method is a descent one if (24) holds. The most general result has been obtained by Gilbert and Nocedal [10], who have shown that the both PR and HS methods are globally convergent if they generate positive values of  $\beta_k$  and if (25) holds. This result is very important because it allows us to develop a great number of useful restart procedures for CG-methods. The reader may see [19] for more details of some of above theoretical results.

**4.1. Lemma:** Consider the CG-method in the form (2) and (3), and let the step-length  $\alpha_k$  be obtained by the line search Algorithm (3.4) with conditions (11) and (12). Suppose that Assumptions 2.1-2.2 hold. Then one has:

$$\sum_{k=0}^{\infty} \alpha_k^2 \left\| d_k \right\|^2 < 0.$$
(26)

**Proof:** Since  $\alpha_k$  is obtained by the line search Algorithm (3.4) with conditions (11)-(12). Then, from (8) and (11) we have

$$f_{k} - f_{k-1} \le -\delta \,\alpha_{k}^{2} \left\| d_{k} \right\|^{2} \le 0.$$
<sup>(27)</sup>

Hence,  $\{f_k\}$  is a decreasing sequence and the sequence  $\{x_k\}$  is contained in F. Hence, Assumptions 2.1-2.2 imply that there exists a constant  $f^*$  such that:

$$\lim_{k \to \infty} f_k = f^*.$$
<sup>(28)</sup>

From (28), we have:

$$\sum_{k=0}^{\infty} \left( f_{k-1} - f_k \right) < +\infty.$$
<sup>(29)</sup>

This together with (27) implies that (26) holds.

**4.2. Lemma:** For the new proposed algorithm, defined in (21), if there exists a constant  $\varepsilon > 0$  such that:

$$\|g_k\| \ge \varepsilon, \quad \forall k \ge 0, \tag{30}$$

then there exists a constant M > 0 such that

$$\left\|d_{k}\right\| \leq M, \quad \forall k \geq 0. \tag{31}$$

**Proof:** The proof is same as in [32] except that we have to prove:

$$t = 2 \frac{\left\|y_{k-1}\right\|^2}{s_{k-1}^T y_{k-1}} = \frac{2}{\alpha_{k-1}} \frac{\left\|y_{k-1}\right\|^2}{d_{k-1}^T y_{k-1}} \ge 0$$
(32a)

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and

$$\gamma_k = \frac{y_{k-1}^T s_{k-1}}{y_{k-1}^T y_{k-1}} \ge 0, \text{ since } y_{k-1}^T s_{k-1} > 0, \text{ (B is positive definite)}$$
(32b)

From the line search conditions (11)-(12) and (8), we have

$$y_{k-1}^{T}d_{k-1} = g_{k}^{T}d_{k-1} - g_{k-1}^{T}d_{k-1} \ge -(1-\sigma)g_{k-1}^{T}d_{k-1} = (1-\sigma)\|g_{k-1}\|^{2}.$$
(33)

since  $0 < \sigma < 1$  implies  $(1 - \sigma)$  is positive. Since  $\alpha_{k-1}$  is also positive step-size obtained by a line search producer, hence the parameter *t* defined in (13c) is positive. This will complete the proof of lemma 4.2. Using the preceding lemmas, we are now ready to give the final convergence results.

**4.3. Theorem:** Suppose that Assumptions 2.1-2.2 hold. Let  $\{x_k\}$  be a sequence of points generated by the new proposed algorithm defined by (21). Then one has

$$\lim_{k \to \infty} \inf \left\| g_k \right\| = 0. \tag{34}$$

**Proof**: We proceed by contradiction. Assume that the conclusion is not true, then there exists a positive constant  $\varepsilon$  such that

$$\left\|\boldsymbol{g}_{k}\right\| \geq \varepsilon, \quad \forall k \geq 0.$$
(35)

If  $\liminf_{k\to\infty} \alpha_k > 0$ , we have from (26) that  $\liminf_{k\to\infty} \|g_k\| = 0$ . This contradicts assumption (35). Suppose that  $\liminf_{k\to\infty} \alpha_k > 0$ . Using Assumptions 2.1-2.2 and from condition (12a), we obtain:

$$-(1-\sigma)g_{k}^{T}d_{k} \leq (g_{k+1}-g_{k})^{T}d_{k} \leq L\alpha_{k} \|d_{k}\|^{2}.$$
(36)

Combining with (8) yields:

$$(1-\sigma) \|g_k\|^2 \le L\alpha_k \|d_k\|^2.$$

$$(37)$$

The above inequality and Lemma 4.2 imply  $\liminf_{k\to\infty} \|g_k\| = 0$ , which contradicts (35). This completes the proof.

#### 5. NUMERICAL RESULTS.

The main work of this section is to report the performance of the new proposed algorithm (say NEW) on a set of test problems. The codes were written in Fortran77 and in double precision arithmetic. All the tests were performed on a PC. Our experiments were performed on a set of (35) nonlinear unconstrained problems that have second derivatives available. These test problems are contributed in CUTE [4] and their details are given in the Appendix. For each test function we have considered 10 numerical experiments with number of variables  $n = 100, 200, \ldots$ , 1000 and we have reported the total amount of each test problem. In order to assess the reliability of our new proposed method, we have tested it against the proposed Al-Bayati and Altae three-term CG-method [2] using the same test problems. All these methods terminate when the following stopping criterion is met:

$$\left\|g_k\right\| \le 10^{-6}.\tag{38}$$

We also force these routines stopped if the iterations exceed 1000 or the number of function evaluations reach 2000 without achieving convergence. We use Algorithm (3.4) as the line search routine satisfying (11) and (12). Tables 5.1 compares some numerical results for NEW method against Al-Bayati and Al-tae [2] three-term CG-method; this table indicates for (n) as a dimension of the problem; (NOI), number of iterations; (NOFG), number of function and gradient evaluations; (TIME), the total time required to complete the evaluation process for each test problem. In Table 5.2 we have compared the percentage performance of the NEW method against Al-Bayati and Altae three-term CG-method [2] taking over all the tools as 100%.

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Table 5.1. Numerical Results for NEW-Algorithm against Algorithm (	(2.5):
For the total of (35) test problems	

$\begin{array}{ c c c c c c } \hline n & NOT & NOFG & TIME & Gmin & n & NOI & NOFG & TIME & Gmin \\ \hline 1 & TOTAL 438 & 805 & 0.43 & 1 & TOTAL 430 & 767 & 0.40 & (seconds) & 2 & TOTAL 335 & 4643 & 0.30 & 2 & TOTAL 330 & 4259 & 0.22 & (seconds) & 3 & TOTAL 40 & 90 & 0.03 & TOTAL 20 & 90 & 0.03 & (seconds) & 4 & 4 & TOTAL 4120 & 6102 & 2.33 & TOTAL 2809 & 4203 & 2.49 & (seconds) & 5 & TOTAL 511 & 5846 & 0.42 & 5 & TOTAL 232 & 444 & 0.06 & (seconds) & 7 & TOTAL 215 & 436 & 0.07 & 7 & TOTAL 232 & 444 & 0.06 & (seconds) & 7 & 7 & 7 & 7 & 7 & 7 & 7 & 7 & 7 & $	Algorithm (2.5)				NEW Algorithm (3.5)					
Image: Construct of the second seco	n	NOI	NOFG		Gmin	n	NOI	NOFG		Gmin
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				TIME					TIME	
TOTAL 4.38       905       0.43       TOTAL 4.30       767       0.40         (seconds)       2       707AL 358       4643       0.30       TOTAL 330       4259       0.22         (seconds)       3       TOTAL 40       90       0.03       TOTAL 40       90       0.03         TOTAL 4120       6102       2.33       TOTAL 2809       4203       2.49         (seconds)       5       TOTAL 504       5801       0.40         (seconds)       6       6       707AL 232       444       0.06         (seconds)       6       6       707AL 335       6178       2.96       7         7       707AL 335       6178       2.96       7       707AL 301       3590       1.44         (seconds)       7       707AL 40       90       0.06       707AL 198       361       0.05         (seconds)       7       707AL 40       90       0.06       707AL 40       90       0.06         (seconds)       10       707AL 40       90       0.06       (seconds)       10         10       10       707AL 40       90       0.06       (seconds)       10         11       707AL 213 </td <td>1</td> <td></td> <td></td> <th></th> <td>0 10</td> <td>1</td> <td></td> <td></td> <td></td> <td>0.40</td>	1				0 10	1				0.40
1 Seconds)       2         TTAL 358 4643       0.30         3       TOTAL 330 4259       0.22         (seconds)       3         3       TOTAL 40 90       0.03         (seconds)       3         4       4         TOTAL 4120       6102       2.33         TOTAL 511       586       0.42         (seconds)       5       TOTAL 504       5801         6       6       TOTAL 232       444       0.06         (seconds)       6       6       6       7         7       TOTAL 335       6178       2.96       TOTAL 198       361       0.06         (seconds)       7       7       7       7       7       7       7         7       TOTAL 335       6178       2.96       TOTAL 198       361       0.05         (seconds)       10       10       10       10       10       10         7       101       10       10       10       10       10         10       10       10       10       10       13       13         10       10       10       10       10       14	TOTAL	. 43 .de)	38 8	805	0.43	TOTAL	43 del	30	767	0.40
TOTAL         358         4643         0.30         TOTAL         330         4259         0.22           (seconds)         (seconds)         TOTAL         40         90         0.03         TOTAL         40         90         0.03           4         (seconds)         (seconds)         TOTAL         28econds)         2.49           (seconds)         (seconds)         (seconds)         0.40         (seconds)           5         TOTAL         511         5846         0.42         TOTAL         504         5801         0.40           (seconds)         6         7 <td>2</td> <td>10.5 /</td> <td></td> <th></th> <td></td> <td>2</td> <td>us /</td> <td></td> <td></td> <td></td>	2	10.5 /				2	us /			
(seconds)         (seconds)           3         TOTAL 40 90 0.03         3           TOTAL 4120 6102 2.33         TOTAL 40 90 0.03         (seconds)           4         TOTAL 4120 6102 2.33         TOTAL 2809 4203 2.49           (seconds)         (seconds)         5           TOTAL 511 5846 0.42         TOTAL 504 5801 0.40           (seconds)         (seconds)           6         6           TOTAL 215 436 0.07         TOTAL 301 3590 1.44           (seconds)         (seconds)           7         TOTAL 335 6178 2.96           7         TOTAL 301 3590 1.44           (seconds)         (seconds)           8         TOTAL 198 361 0.05           (seconds)         (seconds)           9         TOTAL 40 90 0.06           (seconds)         (seconds)           9         TOTAL 40 90 0.06           (seconds)         (seconds)           10         TOTAL 40 90 0.06           (seconds)         (seconds)           11         TOTAL 217 0.098           (seconds)         (seconds)           12         TOTAL 210 0.04           13         TOTAL 20 50 0.02           (seconds)         (seconds)	TOTAL	. 35	58 46	543	0.30	TOTAL	33	30 4	4259	0.22
3         TOTAL 40         90         0.03         TOTAL 40         90         0.03           4         4         4         70TAL 4120         6102         2.33         TOTAL 2809         4203         2.49           (seconds)         5         5         70TAL 511         5846         0.42         5644         0.40           (seconds)         6         6         7         <	(secon	ıds)				(secon	ds)			
101AD       40       50       0.03         4       (seconds)       4         4       4         4       4         4       233       TOTAL 2809       4203       2.49         (seconds)       (seconds)       5       5       0.42       TOTAL 504       5801       0.40         (seconds)       6       6       7       TOTAL 215       436       0.07       TOTAL 232       444       0.06         (seconds)       7       7       TOTAL 335       6178       2.96       TOTAL 301       3590       1.44         (seconds)       (seconds)       8       7       8       0.05       (seconds)       1.44       (seconds)       1.44       (seconds)       1.44       1.44       1.44       1.44       1.44       1.44       1.44       1.44       1.44       1.44       1.44       1.45       1.45       1.44       1.45       1.44       1.45       1.44       1.45       1.44       1.	3 	/	10	0.0	0 0 2	3 	,	10	0.0	0 0 2
4       TOTAL 4120       6102       2.33       TOTAL 2809       4203       2.49         TOTAL 511       5846       0.42       TOTAL 504       5801       0.40         (seconds)       6       TOTAL 215       436       0.07       TOTAL 232       444       0.06         (seconds)       6       TOTAL 335       6178       2.96       TOTAL 301       3590       1.44         (seconds)       7       TOTAL 143       293       0.04       8       7       7         TOTAL 40       90       0.06       TOTAL 40       90       0.06       (seconds)       10         9       TOTAL 245       444       0.03       TOTAL 247       440       0.04         (seconds)       10       TOTAL 247       440       0.04       (seconds)       11         10       TOTAL 245       444       0.03       TOTAL 247       440       0.04         (seconds)       10       TOTAL 247       440       0.04       (seconds)       12         11       TOTAL 211       2104       0.91       TOTAL 237       0.04       (seconds)       13         12       10       11       TOTAL 102       0.03	(secon	ids)	ŧŪ	90	0.03	(secon	ds)	ŧU	90	0.03
TOTAL         4120         6102         2.33         TOTAL         2809         4203         2.49           (seconds)         5         5         5         5         5         5         6           TOTAL         215         436         0.42         TOTAL         504         5801         0.40           (seconds)         6         6         7	4	,				4	,			
(seconds)       (seconds)         5       TOTAL 511 5846       0.42         7       TOTAL 215 436       0.07         6       TOTAL 215 436       0.07         7       TOTAL 335 6178       2.96         7       TOTAL 301 3590       1.44         (seconds)       (seconds)         8       TOTAL 143 293       0.04         7       TOTAL 198 361       0.05         (seconds)       (seconds)       8         8       TOTAL 143 293       0.04       TOTAL 198 361       0.05         (seconds)       (seconds)       8       0.05       (seconds)         9       TOTAL 40 90       0.06       TOTAL 40 90       0.06         (seconds)       10       TOTAL 247 440       0.04         (seconds)       10       10       10         104       11       11       11       11         107AL 211 2104       0.91       10       0.98       (seconds)         12       12       12       12       13       13         13       TOTAL 20       50       0.02       13       13         14       15       15       16       16	TOTAL	41	6 20	5102	2.33	TOTAL	280	)9 4	4203	2.49
S         TOTAL         511         5846         0.42         TOTAL         504         5801         0.40           (seconds)         6         6         6         7	(secon	ıds)				(secon	ds)			
(seconds)         (seconds)         (seconds)           6         TOTAL 215         436         0.07         TOTAL 232         444         0.06           (seconds)         7         TOTAL 335         6178         2.96         TOTAL 301         3590         1.44           (seconds)         8         7         TOTAL 143         293         0.04         TOTAL 198         361         0.05           (seconds)         9         7         TOTAL 40         90         0.06         (seconds)           9         TOTAL 40         90         0.06         (seconds)         0.04         (seconds)           10         TOTAL 245         444         0.03         TOTAL 247         440         0.04           (seconds)         10         TOTAL 213         2170         0.98         (seconds)           11         TOTAL 211         2104         0.91         TOTAL 232         10.98         (seconds)           12         TOTAL 615         967         0.20         TOTAL 537         898         0.18           (seconds)         13         13         13         13         13         14         14           TOTAL 109         223         0.04	о Тотат	. 51	1 58	346	0.42	S TOTAI	5(	)4 "	5801	0.40
	(secon	.ds)			0.12	(secon	ds)			0.10
TOTAL         215         436         0.07         TOTAL         232         444         0.06           (seconds)         7 <t< td=""><td>6</td><td></td><td></td><th></th><td></td><td>6</td><td></td><td></td><td></td><td></td></t<>	6					6				
(Seconds)       7         7       TOTAL 335 6178       2.96         8       TOTAL 301 3590       1.44         (seconds)       8         TOTAL 143 293       0.04       TOTAL 198 361       0.05         (seconds)       9       9       7         TOTAL 40 90       0.06       TOTAL 40 90       0.06         (seconds)       10       TOTAL 40 90       0.06         10       TOTAL 247       440 0.04       0.04         (seconds)       10       TOTAL 247 440       0.04         (seconds)       (seconds)       10       10         TOTAL 211 2104       0.91       TOTAL 213 2170       0.98         (seconds)       (seconds)       (seconds)       12         TOTAL 615 967       0.20       TOTAL 537 898       0.18         (seconds)       (seconds)       13       13         TOTAL 102       20       0.04       TOTAL 102       208       0.03         (seconds)       (seconds)       15       15       15       15         TOTAL 149       272       0.07       TOTAL 148       270       0.07         (seconds)       16       16       16 <td< td=""><td>TOTAL</td><td>. 21</td><td>.5 4</td><th>36</th><td>0.07</td><td>TOTAL</td><td>23</td><td>32 4</td><td>444</td><td>0.06</td></td<>	TOTAL	. 21	.5 4	36	0.07	TOTAL	23	32 4	444	0.06
TOTAL       335       6178       2.96       TOTAL       301       3590       1.44         (seconds)       8       8       0.04       TOTAL       198       361       0.05         (seconds)       9       0.04       TOTAL       198       361       0.05         (seconds)       9       0.06       TOTAL       40       90       0.06         (seconds)       10       TOTAL       247       440       0.04         (seconds)       11       TOTAL       247       440       0.04         (seconds)       11       TOTAL       213       2170       0.98         (seconds)       (seconds)       12       12       0.98       (seconds)         12       TOTAL       615       967       0.20       TOTAL       20       50       0.02         (seconds)       13       13       TOTAL       100       0.02       (seconds)       0.03<	(secon	ias)				(secon 7	as)			
(seconds)         (seconds)           8         8           TOTAL 143         293         0.04         TOTAL 198         361         0.05           (seconds)         9         70TAL 40         90         0.06         TOTAL 40         90         0.06           (seconds)         10         TOTAL 40         90         0.06         (seconds)         0           10         TOTAL 245         444         0.03         TOTAL 247         440         0.04           (seconds)         (seconds)         TOTAL 213         2170         0.98           (seconds)         (seconds)         (seconds)         0         0.98           (seconds)         (seconds)         12         0.98         (seconds)           12         TOTAL 615         967         0.20         TOTAL 537         898         0.18           (seconds)         (seconds)         (seconds)         13         13         13           TOTAL 109         223         0.04         TOTAL 102         208         0.03           (seconds)         16         16         16         16         16           TOTAL 111         232         0.06         (seconds)         16 <td>TOTAL</td> <td>33</td> <td>35 61</td> <th>78</th> <td>2.96</td> <td>TOTAL</td> <td>3(</td> <td>)1 3</td> <td>3590</td> <td>1.44</td>	TOTAL	33	35 61	78	2.96	TOTAL	3(	)1 3	3590	1.44
8         8           TOTAL 143         293         0.04         TOTAL 198         361         0.05           9         TOTAL 40         90         0.06         TOTAL 40         90         0.06           (seconds)         10         TOTAL 245         444         0.03         TOTAL 247         440         0.04           (seconds)         10         TOTAL 247         440         0.04         (seconds)           11         TOTAL 211         2104         0.91         TOTAL 213         2170         0.98           (seconds)         (seconds)         12         TOTAL 615         967         0.20         TOTAL 537         898         0.18           (seconds)         (seconds)         13         13         TOTAL 102         208         0.02           12         TOTAL 20         50         0.02         TOTAL 102         208         0.03           (seconds)         (seconds)         (seconds)         14         14         14           TOTAL 109         223         0.04         TOTAL 102         208         0.03           (seconds)         (seconds)         15         15         15           TOTAL 149         272	(secon	ıds)				(secon	ds)			
TOTAL       143       293       0.04       TOTAL       198       361       0.05         (seconds)       9       70TAL       40       90       0.06       TOTAL       40       90       0.06         10       10       10       TOTAL       247       440       0.04       (seconds)         11       TOTAL       245       444       0.03       TOTAL       247       440       0.04         (seconds)       10       TOTAL       247       440       0.04       (seconds)         11       TOTAL       245       444       0.91       TOTAL       247       440       0.04         (seconds)       (seconds)       10       TOTAL       213       2170       0.98         (seconds)       (seconds)       (seconds)       13       13       13         TOTAL       20       50       0.02       TOTAL       20       50       0.02         (seconds)       14       14       14       14       14       14       14       14       14       14       14       14       14       14       14       15       15       15       15       15       15 <td< td=""><td>8</td><td></td><td></td><th></th><td>0.04</td><td>8</td><td></td><td></td><td>2.61</td><td>0.05</td></td<>	8				0.04	8			2.61	0.05
9       9       0.06       TOTAL 40 90 0.06       0.06         10       10       TOTAL 40 90 0.06       (seconds)         10       10       TOTAL 247 440 0.04       0.04         (seconds)       10       TOTAL 247 440 0.04       0.04         (seconds)       11       TOTAL 213 2170 0.98       0.98         (seconds)       (seconds)       11       11         TOTAL 211 2104 0.91       TOTAL 213 2170 0.98       0.98         (seconds)       (seconds)       12       12         TOTAL 615 967 0.20       TOTAL 537 898 0.18       0.18         (seconds)       (seconds)       13       13         TOTAL 20 50 0.02       TOTAL 20 50 0.02       0.02       (seconds)         14       14       TOTAL 102 208 0.03       0.03         (seconds)       (seconds)       15       15         TOTAL 109 223 0.06       TOTAL 111 232 0.06       0.06         (seconds)       16       16       17         TOTAL 473 910 0.10       TOTAL 503 983 0.10       0.07         (seconds)       18       18       17         TOTAL 661 8083 0.75       TOTAL 580 6812 0.58       0.58         (seconds)       19       1	TOTAL	. 14 .de)	13 2	.93	0.04	TOTAL	da) 1	98	361	0.05
TOTAL         40         90         0.06         TOTAL         40         90         0.06           (seconds)         10         10         10         10         10           TOTAL         245         444         0.03         TOTAL         247         440         0.04           (seconds)         10         TOTAL         247         440         0.04           (seconds)         (seconds)         11         TOTAL         2170         0.98           (seconds)         (seconds)         12         TOTAL         537         898         0.18           (seconds)         (seconds)         13         TOTAL         20         50         0.02           13         13         13         (seconds)         14         14           TOTAL         109         223         0.04         TOTAL         102         208         0.03           14         14         14         14         15         15         15         15         16         16         16         16         16         16         16         16         17         17         17         17         17         17         17         17         17 <td>9</td> <td>ius j</td> <td></td> <th></th> <td></td> <td>9</td> <td>us)</td> <td></td> <td></td> <td></td>	9	ius j				9	us)			
(seconds)       (seconds)         10       10         TOTAL 245       444       0.03       TOTAL 247       440       0.04         (seconds)       (seconds)       11       11       11         TOTAL 211       2104       0.91       TOTAL 213       2170       0.98         (seconds)       (seconds)       12       12       12       13         TOTAL 615       967       0.20       TOTAL 537       898       0.18         (seconds)       (seconds)       13       13       13         TOTAL 20       50       0.02       TOTAL 20       50       0.02         (seconds)       14       14       14       14         TOTAL 109       223       0.04       TOTAL 102       208       0.03         (seconds)       15       15       15       15       15         TOTAL 111       232       0.06       (seconds)       16       16         TOTAL 473       910       0.10       TOTAL 503       983       0.10         (seconds)       17       17       17       17       17         TOTAL 473       910       0.10       TOTAL 503       983 <td>TOTAL</td> <td>. 4</td> <td>±0</td> <th>90</th> <td>0.06</td> <td>TOTAL</td> <td>4(</td> <td>)</td> <td>90</td> <td>0.06</td>	TOTAL	. 4	±0	90	0.06	TOTAL	4(	)	90	0.06
10       10         TOTAL 245       444       0.03       TOTAL 247       440       0.04         (seconds)       (seconds)       11       11       11         TOTAL 211       2104       0.91       TOTAL 213       2170       0.98         (seconds)       (seconds)       12       0.20       TOTAL 537       898       0.18         12       12       TOTAL 20       50       0.20       TOTAL 537       898       0.18         (seconds)       (seconds)       13       TOTAL 20       50       0.02       (seconds)         13       TOTAL 102       208       0.03       (seconds)       0.03       (seconds)         14       14       14       TOTAL 102       208       0.03       (seconds)         14       11       232       0.06       TOTAL 111       232       0.06         (seconds)       15       15       TOTAL 148       270       0.07       (seconds)         16       TOTAL 149       272       0.07       TOTAL 148       270       0.07         (seconds)       (seconds)       (seconds)       10       10       10       10         17       TOTAL	(secon	ıds)				(secon	ds)			
101AL       243       444       0.03       101AL       247       440       0.04         (seconds)       11       11       11       11       0.98       (seconds)         12       12       12       0.96       0.02       TOTAL       537       898       0.18         13       13       13       13       0.02       TOTAL       20       50       0.02         14       14       14       14       0.91       0.03       0.03       0.03       0.03         15       15       0.06       TOTAL       11       232       0.06       0.07         16       15       15       15       0.07       16       0.07       0.07         16       107AL       149       272       0.07       16       0.07       0.07         16       17       16       17       17       0.07       0.07       0.07         (seconds)       16       17       17       17       0.07       0.07         (seconds)       16       17       17       17       17       0.07       0.07         (seconds)       16       17       148       270	10	2/			0 0 2	10	2	1 -7	4.4.0	0.04
11       11       11       11       TOTAL 211 2104       0.91       TOTAL 213 2170       0.98         (seconds)       12       12       TOTAL 615 967       0.20       TOTAL 537 898       0.18         (seconds)       13       TOTAL 20 50       0.02       TOTAL 20 50       0.02         (seconds)       13       TOTAL 20 50       0.02       (seconds)       0.02         (seconds)       14       14       102       208       0.03         (seconds)       (seconds)       (seconds)       0.03       (seconds)         14       14       102       208       0.03         (seconds)       (seconds)       (seconds)       0.03         15       TOTAL 111 232       0.06       TOTAL 111 232       0.06         (seconds)       16       16       16       0.07       (seconds)         16       17       17       17       0.07       (seconds)       0.10         17       174       17       17       17       0.10       17         17       174       18       18       18       0.10       0.58         (seconds)       19       19       19       19       149	(secon	uds)	±5 4	44	0.03	(secon	⊿' ds)	± /	440	0.04
TOTAL 211       2104       0.91       TOTAL 213       2170       0.98         (seconds)       12       12       12       12       13         TOTAL 615       967       0.20       TOTAL 537       898       0.18         (seconds)       (seconds)       13       13       13         TOTAL 20       50       0.02       TOTAL 20       50       0.02         (seconds)       14       14       14       14         TOTAL 109       223       0.04       TOTAL 102       208       0.03         (seconds)       15       15       15       15       15         TOTAL 111       232       0.06       TOTAL 111       232       0.06         (seconds)       16       16       16       17       16         TOTAL 149       272       0.07       TOTAL 148       270       0.07         (seconds)       17       17       17       17       17         TOTAL 473       910       0.10       TOTAL 503       983       0.10         (seconds)       18       18       18       0.58       19         TOTAL 149       394       0.03       TOTAL 149 <td>11</td> <td>.u.o /</td> <td></td> <th></th> <td></td> <td>11</td> <td></td> <td></td> <td></td> <td></td>	11	.u.o /				11				
(seconds)       (seconds)         12       TOTAL 615 967       0.20       TOTAL 537 898       0.18         (seconds)       (seconds)       13       13       13         TOTAL 20 50       0.02       TOTAL 20 50       0.02       (seconds)         14       13       14       14         TOTAL 109 223       0.04       TOTAL 102 208       0.03         (seconds)       (seconds)       15       15         TOTAL 111 232       0.06       TOTAL 111 232       0.06         (seconds)       16       16       16         TOTAL 4473 910       0.10       TOTAL 503 983       0.10         (seconds)       17       17       17         TOTAL 473 910       0.10       TOTAL 503 983       0.10         (seconds)       (seconds)       18       18         TOTAL 661 8083       0.75       TOTAL 580 6812       0.58         (seconds)       19       19       19       0.03	TOTAL	_ 21	1 2	2104	0.91	TOTAL	23	L3 2	2170	0.98
12       12       TOTAL 615 967       0.20       TOTAL 537 898       0.18         (seconds)       13       13       13       13       13         TOTAL 20 50       0.02       TOTAL 20 50       0.02       0.02       0.02         (seconds)       14       14       14       14         TOTAL 109 223       0.04       TOTAL 102 208       0.03         (seconds)       (seconds)       15       15         TOTAL 111 232       0.06       TOTAL 111 232       0.06         (seconds)       16       16       17         TOTAL 473 910       0.10       TOTAL 503 983       0.10         (seconds)       (seconds)       17       17         TOTAL 473 910       0.10       TOTAL 503 983       0.10         (seconds)       (seconds)       17       17         TOTAL 473 910       0.10       TOTAL 503 983       0.10         (seconds)       18       18       10       18         TOTAL 661 8083       0.75       TOTAL 580 6812       0.58         (seconds)       19       19       149       394       0.03	(secon	ıds)				(secon	ds)			
(seconds)       (seconds)       13         TOTAL 20 50 0.02       TOTAL 20 50 0.02         (seconds)       (seconds)         14       14         TOTAL 109 223 0.04       TOTAL 102 208 0.03         (seconds)       (seconds)         15       15         TOTAL 111 232 0.06       TOTAL 111 232 0.06         (seconds)       16         TOTAL 149 272 0.07       TOTAL 148 270 0.07         (seconds)       (seconds)         17       17         TOTAL 473 910 0.10       TOTAL 503 983 0.10         (seconds)       (seconds)         18       18         TOTAL 661 8083 0.75       TOTAL 580 6812 0.58         (seconds)       19         19       19         TOTAL 149 394 0.03       0.03	TOTAT	. 61	5 9	67	0 20		5	37	898	0 18
13       13         TOTAL       20       50       0.02       TOTAL       20       50       0.02         (seconds)       14       14       14       14       14         TOTAL       109       223       0.04       TOTAL       102       208       0.03         (seconds)       (seconds)       15       15       0.06       TOTAL       111       232       0.06         (seconds)       15       15       TOTAL       111       232       0.06       (seconds)         16       16       16       16       0.07       (seconds)       0.07       (seconds)         17       17       17       17       0.007       (seconds)       0.10       (seconds)         18       18       18       18       18       0.10       (seconds)       0.58         (seconds)       19       19       19       0.03       149       394       0.03	(secon	.ds)		0,	0.20	(secon	ds)		0,00	0.10
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	TOTAT	, 14	19 3	394	0.03	19 TOTAL	14	19	394	0.03

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(seconds)			(seconds)		
20			20		
TOTAL 374	744	0.08	TOTAL 395	774	0.08
(seconds)			(seconds)		
21			21		
TOTAL 40	90	0 03	TOTAL 40	90	0 03
(seconds)	20	0.05	(seconds)	50	0.05
22			22		
	14000	1 0 0		12202	0 0 0
	14900	1.02		13203	0.98
(seconds)			(seconds)		
23			23		
TOTAL 246	458	0.15	TOTAL 238	440	0.15
(seconds)			(seconds)		
24			24		
TOTAL 201	412	0.05	TOTAL 201	412	0.05
(seconds)			(seconds)		
25			25		
TOTAL 272	488	0.06	TOTAL 233	421	0.06
(seconds)			(seconds)		
26			26		
TOTAL 200	432	0 05	TOTAL 200	432	0 05
(seconds)	452	0.05	(seconds)	452	0.05
	100	0 0 0		100	0.00
TOTAL 39	108	0.03	TOTAL 39	108	0.03
(seconds)			(seconds)		
28			28		
TOTAL 61	824	0.30	TOTAL 61	824	0.30
(seconds)			(seconds)		
29			29		
TOTAL 30	70	0.03	TOTAL 30	70	0.03
(seconds)			(seconds)		
30			30		
TOTAL 211	2104	0.91	TOTAL 153	1370	0.84
(seconds)	2201	0.02	(seconds)	2070	0.01
31			31		
	170/	0 01		000	0 0 0
(gogonda)	1/94	0.01	(accorda)	900	0.08
(seconds)			(seconds)		
32	2.0	0 01	32	2.0	0 01
TOTAL 10	30	0.01	TOTAL 10	30	0.01
(seconds)			(seconds)		
33			33		
TOTAL 355	675	0.09	TOTAL 353	663	0.07
(seconds)			(seconds)		
34			34		
TOTAL 90	110	0.02	TOTAL 90	110	0.02
(seconds)			(seconds)		
35			35		
TOTAL 195	437	0.05	TOTAL 288	478	0.06
(seconds)			(seconds)		
Total			Total		
OF 25 1/122	61054	10 54	OF 25 11000	50007	10 00
	01934	12.04		5230/	T0.00
Test			Test		
Fun.			Fun.		

 Table 5.2.
 Percentage performance of NEW-Algorithm against Algorithm (2.5)

Tools	Algorithm (2.5)	NEW (Algorithm 3.5)
NOI	100%	78.5%
NOFG	100%	84.5%
TIME	100%	80.3%

It is clear from Table (5.2) that taking, over all, the Tools as a 100% for the Al-Bayati and Altae three-term CGmethod, namely algorithm (2.5), the NEW-Algorithm has an improvement, in about (21.5%) NOI; (16.5%) NOFG and (19.7%) TIME.

## CONCLUSIONS:

Taking everything into consideration the new proposed scaled three-term CG-method have been obtained very significant development as we have expected, we think that, for all the specific problems, the enhancement of the new proposed method is very robust. However, we know that CG-methods are sensitive to the order of interpolation; therefore, we have recommend a modified perfect cubic interpolation over the standard quadratic one in our implementations. Hence, we believe that the new method is a valid approach for the problems and has its own potential. Also, the effectiveness of this new proposed method depends on the robustness set of selected scaling criteria and several selected sets of restating techniques used in this research besides the selected set of test functions.

## ACKNOWLEDGEMENTS

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## APPENDIX

The details of the test functions, used in this paper, can be found in [4]. The numbers (1-35) in Table 5.1 indicate to:

- 1- Extended Trigonometric Function.
- 2- Extended Penalty Function.
- 3- Raydan 2 Function.
- 4- Diagonal2 Function.
- 5- Generalized Tridiagonal-1 Function.
- 6- Extended Tridiagonal-1 Function.
- 7- Extended 3-Exponential Terms Function.
- 8- Diagonal4 Function.
- 9- Diagonal5 Function.
- 10- Extended Himmelblau Function.
- 11- Extended PSC1 Function.
- 12- Extended Block Diagonal BD1 Function.
- 13- Extended EP1 Function.
- 14- DIXMAANA CUTE- Function.
- 15- DIXMAANB CUTE- Function.
- 16- DIXMAANC CUTE- Function.
- 17- Broyden Tri-diagonal Function.
- 18- EDENSCH CUTE- Function.

- 19- VARDIM CUTE- Function. 20- LIARWHD CUTE- Function. 21- DIAGONAL 6 Function. 22- ENGVAL1 CUTE- Function. 23- DENSCHNA CUTE- Function. 24- DENSCHNB CUTE- Function. 25- DENSCHNF CUTE- Function. 26- Generalized Quartic GQ1 function. 27- Diagonal 7 Function. 28- Diagonal 8 Function. 29- Full Hessian Function. 30- SINCOS Function. 31- Generalized quartic GO2 function. 32- ARGLINB CUTE-Function. 33- FLETCHCR CUTE-Function. 34- HIMMELBG CUTE-Function.
- 35- HIMMELBH CUTE-Function.

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